

Original Research Paper

New About the Balancing of Thermal Motors

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Abstract: The paper presents a new method of balancing the thermal motors, the method that perfectly fits the engines with modern internal combustion. This new constructive method imposes a new in-line engine design in order to better balance it, thus achieving a static balancing and total dynamics of the new type of internal combustion heat engine. The method can also be extended to external combustion thermal engines.

Keywords: Robots, Mechatronic Systems, Structure, Dynamics, Dynamics Systems, Machines, Engines, Thermal Engines, Engines Balancing

Introduction

This paper wants to complement an important aspect of internal combustion engines, as these engines are still working massively in global transport, and probably will do so for a long time, even if the electric motors slowly appeared multiplying the old Otto-type internal combustion engine or diesel.

If over the past 50 years, we witnessed a crisis of classical fossil fuels, due to increasing consumption, while petroleum reserves diminished by their eyes, today the expectations are quite different as the conditions and planetary resources have changed completely. Classic and fuel-powered games are today completely different from those in the last 50 years, precisely because of the discovery of new energy resources including fossil-powered planets.

The energy crisis that began in the 1970s and 1980s was completely overcome, initially through the construction of nuclear fission power plants, which at that time was a necessary evil because they stopped the global energy crisis that led to other social, economic crises ... We had in this way to restructure our energy resources, to switch the majority of public transport to electric motors, but to discover new energy sources. Today we can breathe easy because we already have more energy resources than needed, and huge reserves for the future, but still many other major prospects. Renewable energy resources, mostly solar and wind power, have now grown, resources that supply oil and natural gas, creating the possibility of storing oil reserves or even switching to 100% renewable energy systems in the future. In addition, new oil reserves have been discovered at the planetary level which has even led to the relaxation of this area. There have also been added

new natural gas resources that can be used for the next 2,000 years in the future, given the fact that other energy resources will not be used, and even more so in the current conditions in which energy is already acquired mostly from wind, sun, water, and nuclear. We can say that we are well, very well, given the fact that the gas reserves of the planet have increased due to the exploitation of deep-shale gas, through modern extraction technologies. Today's gas can easily cover gas needs for at least two or even three thousand years at least, and not just because three large factories have already been built to convert gas into gasoline, diesel, kerosene or any type the desired oil fuel, and that in enormous quantities, and by multiplying in the future these special refineries will be able to obtain huge quantities of any kind of petroleum fuel only from the planetary shale gas reserves. We can sleep so we will have two or three thousand years of gas reserves, and any kind of oil fuel. Even though the number of vehicles has increased greatly and the specific consumption of fuel has decreased due to permanent refurbishment in this priority area.

A few years ago, a British company managed to get fossil fuels only from the atmosphere and energy, recovering the carbon products existing today in the air. Such a plant has not yet appeared because the technologies are too expensive and we already have fossil reserves at our discretion for several thousand years, given that we have been able to obtain most energy from water, sun, wind or nuclear.

Recently, a prestigious university in Switzerland managed to obtain superior fuels only from water and solar energy through simple, technologically simple processes that will only require a large amount of space allotted to produce continually high-quality kerosene

from water and solar energy. So if there are still classical fuels, they can be re-infused just by the water and solar energy. We can now say that the games are already being made, especially as more and more electric motors have appeared on motor vehicles, some of them using hydrogen as a fuel, which in turn is a major energy resource on a massive scale, already massively implemented, and with great prospects for the future.

Under these new conditions, the necessity of continuing the studies on the thermal engines with the aim of their permanent improvement appears (Aabadi, 2019; Antonescu and Petrescu, 1985; 1989; Antonescu *et al.*, 1985a; 1985b; 1986; 1987; 1988; 1994; 1997; 2000a; 2000b; 2001; Aversa *et al.*, 2017a; 2017b; 2017c; 2017d; 2017e; 2016a; 2016b; 2016c; 2016d; 2016e; 2016f; 2016g; 2016h; 2016i; 2016j; 2016k; 2016l; 2016m; 2016n; 2016o; Cao *et al.*, 2013; Dong *et al.*, 2013; Comanescu, 2010; Franklin, 1930; He *et al.*, 2013; Lee, 2013; Lin *et al.*, 2013; Liu *et al.*, 2013; Padula and Perdereau, 2013; Perumaal and Jawahar, 2013; Petrescu, 2011; 2015a; 2015b; Petrescu and Petrescu, 1995a; 1995b; 1997a; 1997b; 1997c; 2000a; 2000b; 2002a; 2002b; 2003; 2005a; 2005b; 2005c; 2005d; 2005e; 2011a; 2011b; 2012a; 2012b; 2013a; 2013b; 2013c; 2013d; 2013e; 2016a; 2016b; 2016c; Petrescu *et al.*, 2009; 2016; 2017a; 2017b; 2017c; 2017d; 2017e; 2017f; 2017g; 2017h; 2017i; 2017j; 2017k; 2017l; 2017m; 2017n; 2017o; 2017p; 2017q; 2017r; 2017s; 2017t; 2017u; 2017v; 2017w; 2017x; 2017y; 2017z; 2017aa; 2017ab; 2017ac; 2017ad; 2017ae; 2018a; 2018b; 2018c; 2018d; 2018e; 2018f; 2018g; 2018h; 2018i; 2018j; 2018k; 2018l; 2018m; 2018n; Rulkov *et al.*, 2016; Agarwala, 2016; Babayemi, 2016; Ben-Faress *et al.*, 2019; Gusti and Semin, 2016; Mohamed *et al.*, 2016; Wessels and Raad, 2016; Maraveas *et al.*, 2015; Khalil, 2015; Rhode-Barbarigos *et al.*, 2015; Takeuchi *et al.*, 2015; Li *et al.*, 2015; Vernardos and Gantes, 2015; Bourahla and Blakeborough, 2015; Stavridou *et al.*, 2015; Ong *et al.*, 2015; Dixit and Pal, 2015; Rajput *et al.*, 2016; Rea and Ottaviano, 2016; Zurfi and Zhang, 2016 a-b; Zheng and Li, 2016; Buonomano *et al.*, 2016a; 2016b; Faizal *et al.*, 2016; Ascione *et al.*, 2016; Elmeddahi *et al.*, 2016; Calise *et al.*, 2016; Morse *et al.*, 2016; Abouobaida, 2016; Rohit and Dixit, 2016; Kazakov *et al.*, 2016; Alwetaishi, 2016; Riccio *et al.*, 2016a; 2016b; Iqbal, 2016; Hasan and El-Naas, 2016; Al-Hasan and Al-Ghamdi, 2016; Jiang *et al.*, 2016; Sepúlveda, 2016; Martins *et al.*, 2016; Pisello *et al.*, 2016; Jarahi, 2016; Mondal *et al.*, 2016; Mansour, 2016; Al Qadi *et al.*, 2016b; Campo *et al.*, 2016; Samantaray *et al.*, 2016; Malomar *et al.*, 2016; Rich and Badar, 2016; Hirun, 2016; Bucinell, 2016; Nabilou, 2016b; Barone *et al.*, 2016; Bedon and Louter, 2016; Santos and Bedon, 2016; Fontánez *et al.*, 2019; De León *et al.*, 2019; Hypolite *et al.*, 2019; Minghini *et al.*, 2016; Bedon, 2016; Jafari *et al.*, 2016; Orlando and Benvenuti,

2016; Wang and Yagi, 2016; Obaiys *et al.*, 2016; Ahmed *et al.*, 2016; Jauhari *et al.*, 2016; Syahrullah and Sinaga, 2016; Shanmugam, 2016; Jaber and Bicker, 2016; Wang *et al.*, 2016; Moubarek and Gharsallah, 2016; Amani, 2016; Shruti, 2016; Pérez-de León *et al.*, 2016; Mohseni and Tsavdaridis, 2016; Abu-Lebdeh *et al.*, 2016; Serebrennikov *et al.*, 2016; Budak *et al.*, 2016; Augustine *et al.*, 2016; Jarahi and Seifilaleh, 2016; Nabilou, 2016a; You *et al.*, 2016; AL Qadi *et al.*, 2016a; Rama *et al.*, 2016; Sallami *et al.*, 2016; Huang *et al.*, 2016; Ali *et al.*, 2016; Kamble and Kumar, 2016; Saikia and Karak, 2016; Zeferino *et al.*, 2016; Pravettoni *et al.*, 2016; Bedon and Amadio, 2016; Mavukkandy *et al.*, 2016; Yeargin *et al.*, 2016; Madani and Dababneh, 2016; Alhasanat *et al.*, 2016; Elliott *et al.*, 2016; Suarez *et al.*, 2016; Kuli *et al.*, 2016; Waters *et al.*, 2016; Montgomery *et al.*, 2016; Lamarre *et al.*, 2016; Daud *et al.*, 2008; Taher *et al.*, 2008; Zulkifli *et al.*, 2008; Pourmahmoud, 2008; Pannirselvam *et al.*, 2008; Ng *et al.*, 2008; El-Tous, 2008; Akhesmeh *et al.*, 2008; Nachiengtai *et al.*, 2008; Moezi *et al.*, 2008; Boucetta, 2008; Darabi *et al.*, 2008; Semin and Bakar, 2008; Al-Abbas, 2009; Abdulla *et al.*, 2009; Abu-Ein, 2009; Opafunso *et al.*, 2009; Semin *et al.*, 2009a; 2009b; 2009c; Zulkifli *et al.*, 2009; Marzuki *et al.*, 2015; Bier and Mostafavi, 2015; Momta *et al.*, 2015; Farokhi and Gordini, 2015; Khalifa *et al.*, 2015; Yang and Lin, 2015; Demetriou *et al.*, 2015; Rajupillai *et al.*, 2015; Sylvester *et al.*, 2015; Ab-Rahman *et al.*, 2009; Abdulla and Halim, 2009; Zotos and Costopoulos, 2009; Feraga *et al.*, 2009; Bakar *et al.*, 2009; Cardu *et al.*, 2009; Bolonkin, 2009a; 2009b; Nandhakumar *et al.*, 2009; Odeh *et al.*, 2009; Lubis *et al.*, 2009; Fathallah and Bakar, 2009; Marghany and Hashim, 2009; Kwon *et al.*, 2010; Aly and Abuelnasr, 2010; Farahani *et al.*, 2010; Ahmed *et al.*, 2010; Kunanoppadon, 2010; Helmy and El-Taweel, 2010; Qutbodin, 2010; Pattanasethanon, 2010; Fen *et al.*, 2011; Thongwan *et al.*, 2011; Theansuwan and Triratanasirichai, 2011; Al Smadi, 2011; Tourab *et al.*, 2011; Raptis *et al.*, 2011; Momani *et al.*, 2011; Ismail *et al.*, 2011; Anizan *et al.*, 2011; Tsolakis and Raptis, 2011; Abdulla *et al.*, 2011; Kechiche *et al.*, 2011; Ho *et al.*, 2011; Rajbhandari *et al.*, 2011; Aleksic and Lovric, 2011; Kaewnai and Wongwises, 2011; Idarwazeh, 2011; Ebrahim *et al.*, 2012; Abdelkrim *et al.*, 2012; Mohan *et al.*, 2012; Abam *et al.*, 2012; Hassan *et al.*, 2012; Jalil and Sampe, 2013; Jaoude and El-Tawil, 2013; Ali and Shumaker, 2013; Zhao, 2013; El-Labban *et al.*, 2013; Djalel *et al.*, 2013; Nahas and Kozaitis, 2013; Petrescu and Petrescu, 2014a; 2014b; 2014c; 2014d; 2014e; 2014f; 2014g; 2014h; 2014i; 2015a; 2015b; 2015c; 2015d; 2015e; 2016a; 2016b; 2016c; 2016d; Fu *et al.*, 2015; Al-Nasra *et al.*, 2015; Amer *et al.*, 2015; Sylvester *et al.*, 2015b; Kumar *et al.*, 2015; Gupta *et al.*, 2015; Stavridou *et al.*, 2015b; Casadei, 2015; Ge and Xu, 2015; Moretti, 2015; Wang *et al.*, 2015; Petrescu

et al., 2017 af-aj, 2018 o-v; Petrescu, 2015c, 2018 a-b; Petrescu and Petrescu, 2018 a-b).

Materials and Methods

In an internal combustion engine, about one-third of the total fuel power is converted into a useful machine.

Much of the energy is lost in the exhaust. In addition, another important part of the energy consumption is rejected as heating by the cooling system.

The importance of this study is to identify the key factors contributing to heat loss, which can nevertheless be used to minimize heat loss and at the same time improve the strength and efficiency of mechanical components. Loss of stored energy increases with increasing engine speed and engine load and therefore decreases the efficiency of mechanical components.

An important way to reduce the loss of thermal motors is to get a better balance.

In addition, a good balance to achieve silent and long-term operation without high wear, noise and vibration (Petrescu and Petrescu, 2014f; 2014g; 2014h; 2014i).

An important way to reduce the loss of thermal motors is to get a better balance.

On the other hand, the equal parts of the two forces do not give an impulse to produce a dynamic (partial) balance. Instead, only the parts of the two forces that are equal, but have opposite signs, with all that cancels the (static) forces, give a negative moment (load) which unbalanced (partially) dynamic engine.

The solution is taken to balance the overall dynamics of such an engine, doubling the engine (mirror) to get a 180-degree crank in a four-cylinder engine.

Balancing a line engine having a crank with a space of 180 [Deg]

Internal combustion engines (either in four-stroke engines or in two-stroke engines - Otto, Diesel, and Lenoir) are generally the most used engines.

Their balancing problem is extremely important for its smooth operation. There are two possible balancing types: Static and Dynamic.

Total static balancing determines the sum of the inertial forces of a mechanism to be zero. There is also a partial static balancing.

Balancing dynamics means the cancellation of all moments (loads) of the mechanism inertia.

One way to design an inline engine is one with a 180° space.

In this type of engine (regardless of their position, which is most often vertical) for two engine cylinders, they have a partial static imbalance (ie, there is a partial static balancing) and a dynamic imbalance.

Allow me to write the following calculation relationships (1):

$$\left. \begin{aligned} s_B &= r \cdot \sin \phi_1 + l \cdot \sin \phi_2; \\ \ddot{s}_B &= -r \cdot \sin \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\ F = F_B^i &= -m_p \cdot \ddot{s}_B = \\ &= m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\ \sin(\phi_1 + \pi) &= -\sin \phi_1; \sin \phi_2 = \sin \phi_2 \\ s_D &= r \cdot \sin(\phi_1 + \pi) + l \cdot \sin \phi_2; \\ \ddot{s}_D &= -r \cdot \sin(\phi_1 + \pi) \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\ &= r \cdot \sin \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\ F_D^i &= -m_p \cdot \ddot{s}_D \\ &= -m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\ M^i &= a \cdot m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 \end{aligned} \right\} \quad (1)$$

Figure 1 shows the kinematic scheme of such a mechanism (a two-cylinder in-line motor) having a lever of 180°.

Parts of force relations that are equal but have opposite signs cancel each other, producing a partial static equilibrium of the engine.

The other two parts of the force expressions that have the same sign are equal and do not cancel each other, but they come together, producing a static (partial) engine imbalance.

On the other hand, the equal parts of the two forces do not give an impulse to produce a dynamic (partially) engine.

Instead, only the parts of the two forces that are equal but have contradictory signs, although they cancel the (static) forces, give a negative moment (load) that dynamically disturbs the engine.

The solution adopted for a total dynamic equalization of such an engine is duplicating the engine (in a mirror) so as to obtain a 180° lever motor in the four-cylinder engine (Fig. 2).

Balancing a cranking engine with a space of 120 [Deg].

Another type of construction of the line engine is the engine with a space of 120°. In this type of engine (regardless of their position, most often vertical) for a three-cylinder engine, there is a partial static imbalance (ie there is a partial static balancing) and a dynamic imbalance.

Figure 3 shows the kinematic scheme of the mechanism of such an in-line three-cylinder engine, which has a crank with a gap of 120 [deg].

The first component of the force F_B^i is canceled by the first component of the other two forces F_D^i and F_F^i and therefore it produces a static balance (partial), but these first components give a dynamic moment, so we have a dynamic imbalance.

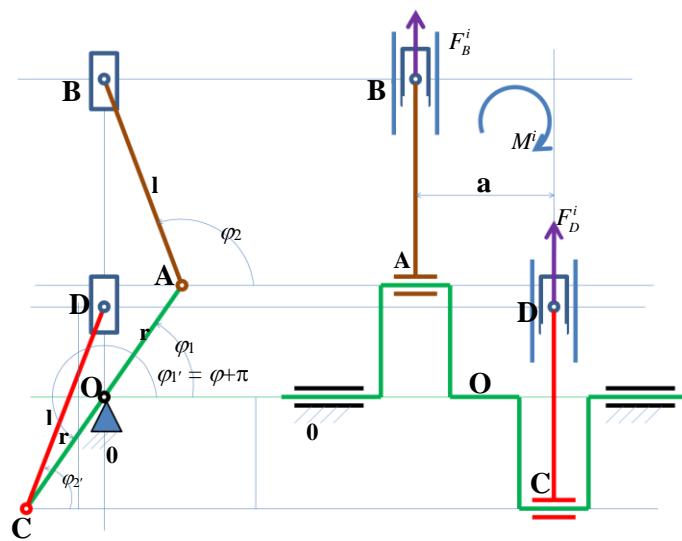


Fig. 1: Kinematic diagram of an vertical engine with two cylinders in line, which has a crank with a gap of 180 [deg]

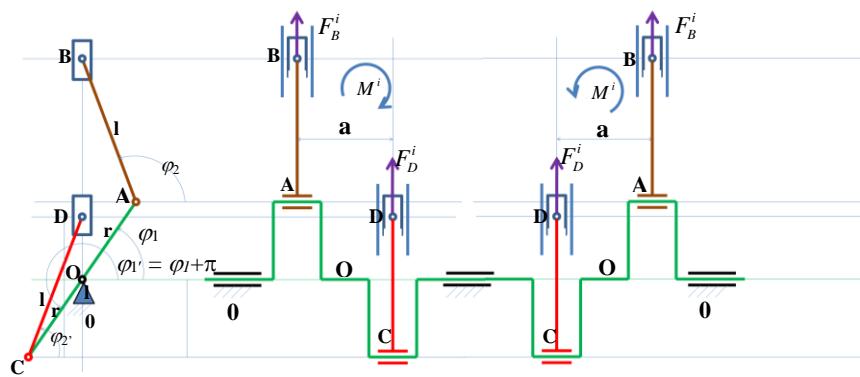


Fig. 2: Kinematic diagram of an vertical engine with four cylinders in line, which has a crank having a gap of 180 [deg]

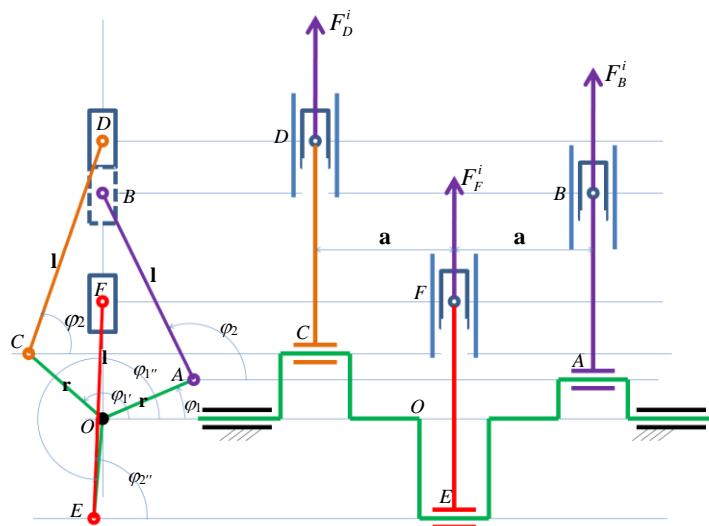


Fig. 3: Kinematic diagram of an vertical engine with three cylinders in line, which has a crank with a gap of 120

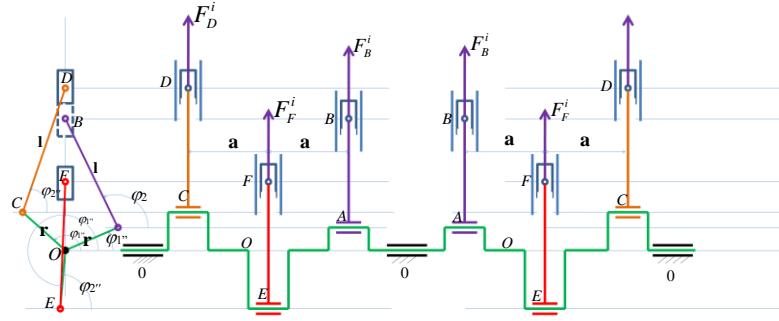


Fig. 4: Kinematic diagram of an vertical engine with six cylinders in line, which has a crank with a gap of 120 [deg]

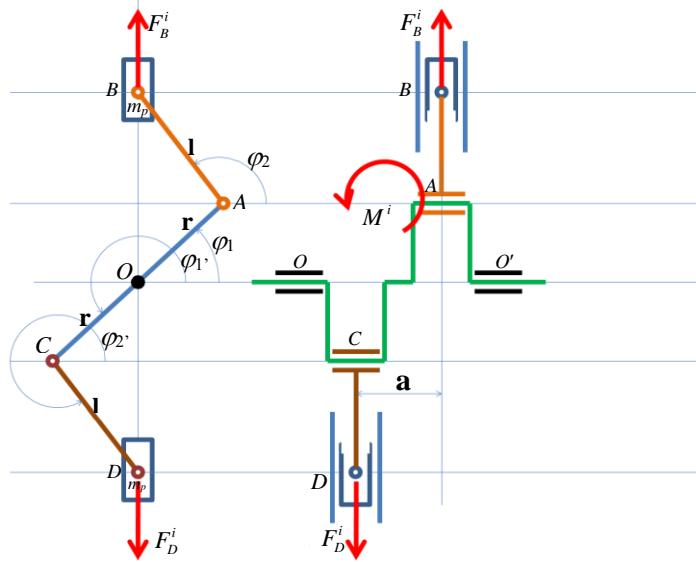


Fig. 5: Kinematic diagram of an engine in line with two opposed cylinders (boxers)

A second component of the force F_D^i is equal and opposite sign of the second component of the force F_F^i , they canceling each other and thus generating a static balancing (partial) additional, but additionally producing a dynamic moment, creating an imbalance additional dynamic. The second component of force F_B^i is added to the third component of the other two forces F_D^i and F_F^i . They produce a static imbalance and gives and a dynamic moment at the same time producing a dynamic imbalance. Adopting an engine solution doubled symmetrically in a mirror (a six-cylinder engine in line with a phase shift of the cranks from 120 [deg]), we achieved an overall dynamic balance (cancellation of all moments given of inertia forces) and a static balance (partial) of two-thirds of the total inertial forces, a balancing which is however superior than of the in-line engines with a phase shift of the cranks from 180 [deg] (Fig. 4).

Shall write following relations of calculation (2):

$$\begin{aligned}
 s_B &= r \cdot \sin \phi_1 + l \cdot \sin \phi_2; \\
 \ddot{s}_B &= -r \cdot \sin \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 F &= F_B^i = -m_p \cdot \ddot{s}_B = m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 s_D &= r \cdot \sin \left(\phi_1 + \frac{2\pi}{3} \right) + l \cdot \sin \phi_2; \\
 \ddot{s}_D &= -r \cdot \sin \left(\phi_1 + \frac{2\pi}{3} \right) \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 = 0.5 \cdot r \cdot \\
 &\sin \phi_1 \cdot \omega_1^2 - 0.866 \cdot r \cdot \cos \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 F_D^i &= -m_p \cdot \ddot{s}_D = -0.5 \cdot m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 \\
 &+ 0.866 \cdot m_p \cdot r \cdot \cos \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 s_F &= r \cdot \sin \left(\phi_1 - \frac{2\pi}{3} \right) + l \cdot \sin \phi_2; \\
 \ddot{s}_F &= -r \cdot \sin \left(\phi_1 - \frac{2\pi}{3} \right) \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 &= 0.5 \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + 0.866 \cdot r \cdot \cos \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 F_F^i &= -m_p \cdot \ddot{s}_F = -0.5 \cdot m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 \\
 &- 0.866 \cdot m_p \cdot r \cdot \cos \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2
 \end{aligned} \tag{2}$$

Remarks: Similarly constructed inline engines with more cylinders, having to crank ever smaller gaps, are obtained by doubling the number of cylinders in the mirror, linear motors with a total dynamic balanced and a partial static balanced that can becoming better. Thus, to an in-line five-cylinder engine with the gap between cranks of $720/5=72$ [deg], one obtains a superior partial static balance and by doubling the engine symmetrically mirrored by making a linear motor with ten cylinders, one obtains a superior partial static balance and an overall dynamic balance.

Thus, constructive and technological requirements are becoming more and more difficult. V motors cannot achieve any static balancing, but not a general dynamics. To improve the dynamics of these higher efficiency motors, see the dynamic and kinematic conditions of the constructive choice of the alpha angle. The most complete solution for balancing the internal combustion engine is considered to be one with the boxer. For the two opposite cylinders, a complete static balancing (inertial forces) and symmetrical doubling in a mirror of the number of cylinders for a four-cylinder engine that resists two or two moments of the total, inertial dynamic force).

Balancing an engine (inline) with opposite cylinders (boxers).

Another type of engine construction is the cylindrical engine in line, called the "boxer" of the cylinders. In this type of engine (regardless of their position, most often vertical) for the two-cylinder engine, there is a total static balancing and a dynamic imbalance. Allow me to write the following calculation relationships (3):

$$\begin{aligned}
 s_B &= r \cdot \sin \phi_1 + l \cdot \sin \phi_2; \\
 \ddot{s}_B &= -r \cdot \sin \phi_1 \cdot \omega_1^2 - l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 F = F_B^i &= -m_p \cdot \ddot{s}_B = m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 \sin(\phi_1 + \pi) &= -\sin \phi_1; \\
 \sin(\phi_2 + \pi) &= -\sin \phi_2 \\
 s_D &= r \cdot \sin(\phi_1 + \pi) + l \cdot \sin(\phi_2 + \pi) \\
 \ddot{s}_D &= -r \cdot \sin(\phi_1 + \pi) \cdot \omega_1^2 - l \cdot \sin(\phi_2 + \pi) \cdot \omega_2^2 \\
 &= r \cdot \sin \phi_1 \cdot \omega_1^2 + l \cdot \sin \phi_2 \cdot \omega_2^2 = -\ddot{s}_B \quad (3) \\
 F_D^i &= -m_p \cdot \ddot{s}_D = m_p \cdot \ddot{s}_B = -F_B^i = -F \\
 &= -m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 - m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 F_D^i + F_B^i &= 0 \text{ dar } M^i \neq 0 \\
 M^i &= a \cdot F_B^i = -a \cdot m_p \cdot \ddot{s}_B \Rightarrow \\
 \Rightarrow M^i &= a \cdot m_p \cdot r \cdot \sin \phi_1 \cdot \omega_1^2 + a \cdot m_p \cdot l \cdot \sin \phi_2 \cdot \omega_2^2 \\
 \text{At the Engine doubled in a mirror} \\
 \sum F^i &= 0 \\
 \sum M^i &= 0
 \end{aligned}$$

Figure 5 shows the kinematic scheme of the mechanism of such a motor (with two opposite cylinders in line) (boxers), (Petrescu and Petrescu, 2014f; 2014g; 2014h; 2014i).

This two-cylinder boxer engine is statically balanced (the sum of the inertial forces must be canceled).

It is only unbalanced dynamic (it has an inertial point different from zero), but it can be dynamically balanced by adding two more cylinders (by symmetry in a mirror) boxers (Fig. 6).

Although it seems to have a larger gauge, though only in four cylinders (two opposite pairs), this type of internal combustion engine heat is almost totally balanced both statically and dynamically. The first engineer to patented a boxer engine was Karl Benz, who presented such a patent of a boxer engine (Fig. 7) in 1896.

In 1923, Max Friz designed and built a BMW 500 cc boxer engine, which is still produced and used today due to its power, low consumption and, in particular, its static and dynamic balancing. German German German German, German Citroen, Chevrolet GM Division (American Louis Louis Chevrolet Division, May 30, 1911) and William Durant, owner of Buick General Motors, German German German division VW.

Another static and dynamic balancing engine, such as Boxer, is the internal combustion engine with the opposite piston (Fig. 8).

Balancing the Rotating Mass

Another type of balancing is that of rotating masses.

The motors (of the thermal motors) are balanced by this model.

It is believed that several masses (concentrates) are attached to a rotary shaft.

The weights are rotated together with the shaft. These may be punctual masses, spheres, etc., however, certain spheres (each of which have mass-centered concentration at the center of gravity) will be considered, as shown in Fig. 9.

The weights are attached to the axis of rotation by different supports, but will only consider the distance theory in the center of each sphere on the axis of the shaft. The perpendicular points passing from the center of each sphere to the axis of the shaft are marked with 1, 2, 3, ... and ... n.

Through these legs, we pulled parallel lines to the x-axis, from which are measured the angles between distances and the horizontal axes. Is measured and the distances of these points measured on the axis of rotation from the origin O of the Cartesian system xOyz (see Fig. 9). Shall be written the amounts moments generated by the forces of inertia of the concentrated masses in relation to the axis Ox, Oy, O'x' and O'y' (system 4). Solve system (4) is carried out with the formulae given by the system (5).

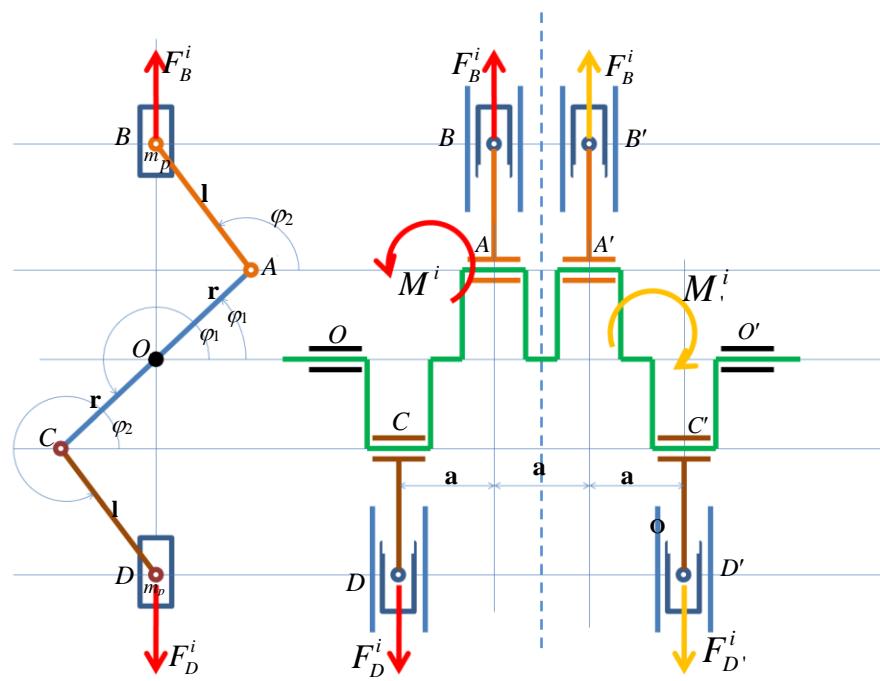


Fig. 6: Kinematic diagram of an engine in line with four opposed cylinders (boxers)

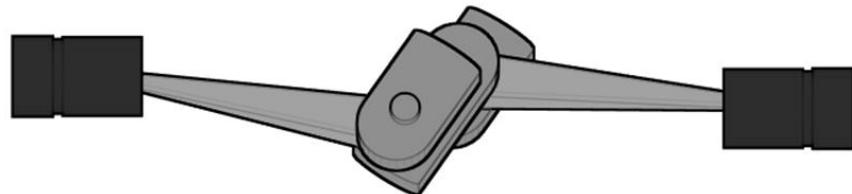


Fig. 7: First boxer engine, patented by Karl Benz

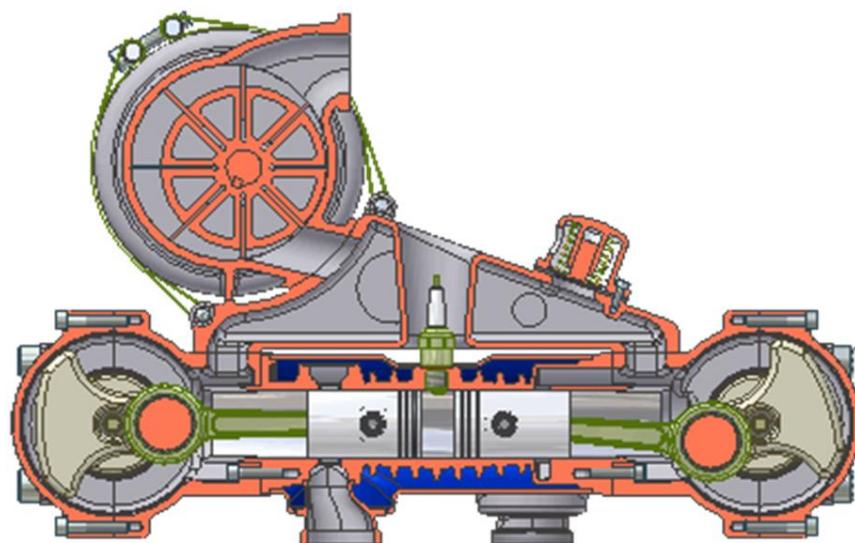


Fig. 8: Kinematic diagram of an engine in line with opposed pistons

Similar to the model of masses concentrated in rotary motion are solved and the balancing of the rotating shafts (Petrescu and Petrescu, 2014f; 2014g; 2014h; 2014i).

$$\left\{ \begin{array}{l} \sum_{j=1}^n (F_j^i \cdot b_j \cdot \sin \phi_j) \\ + F_{II}^i \cdot b \cdot \sin \phi_{II} = 0 \\ \sum_{j=1}^n (F_j^i \cdot b_j \cdot \cos \phi_j) \\ + F_{II}^i \cdot b \cdot \cos \phi_{II} = 0 \\ \sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \sin \phi_j] \\ + F_I^i \cdot b \cdot \sin \phi_I = 0 \\ \sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \cos \phi_j] \\ + F_I^i \cdot b \cdot \cos \phi_I = 0 \end{array} \right. \quad (4)$$

$$\left\{ \begin{array}{l} F_I^i = \frac{1}{b} \cdot \sqrt{\left[\sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \sin \phi_j] \right]^2 + \left[\sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \cos \phi_j] \right]^2} \\ F_{II}^i = \frac{1}{b} \cdot \sqrt{\left[\sum_{j=1}^n (F_j^i \cdot b_j \cdot \sin \phi_j) \right]^2 + \left[\sum_{j=1}^n (F_j^i \cdot b_j \cdot \cos \phi_j) \right]^2} \\ \sin \phi_I = - \frac{\sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \sin \phi_j]}{F_I^i \cdot b}; \\ \cos \phi_I = - \frac{\sum_{j=1}^n [F_j^i \cdot (b - b_j) \cdot \cos \phi_j]}{F_I^i \cdot b} \end{array} \right.$$

$$\left\{ \begin{array}{l} \phi_I = \operatorname{segn}(\sin \phi_I) \cdot \arccos(\cos \phi_I) \\ \sin \phi_{II} = - \frac{\sum_{j=1}^n (F_j^i \cdot b_j \cdot \sin \phi_j)}{F_{II}^i \cdot b}; \\ \cos \phi_{II} = - \frac{\sum_{j=1}^n (F_j^i \cdot b_j \cdot \cos \phi_j)}{F_{II}^i \cdot b} \\ \phi_{II} = \operatorname{segn}(\sin \phi_{II}) \cdot \arccos(\cos \phi_{II}) \end{array} \right. \quad (5)$$

Result and Discussion

Starting with the engine main mechanism in the compressor system (when the motor mechanism is acting from the crank; see the Fig. 10).

The forces of the mechanism can be seen in Fig. 11.

In the diagram below (Fig. 12) we compare this new torque with the classic.

The new torque was determined considering the variation of velocities with forces and forces variation due to velocities (system 6).

In order to achieve an optimum and thus have the maximum possible balance of the moments, which would facilitate the optimal operation of the engine at maximum capacity only with reduced moments and powers, so with reduced fuel consumption and low NOx, it is necessary to pass to a new constructive schema of the internal combustion engine (Fig. 13).

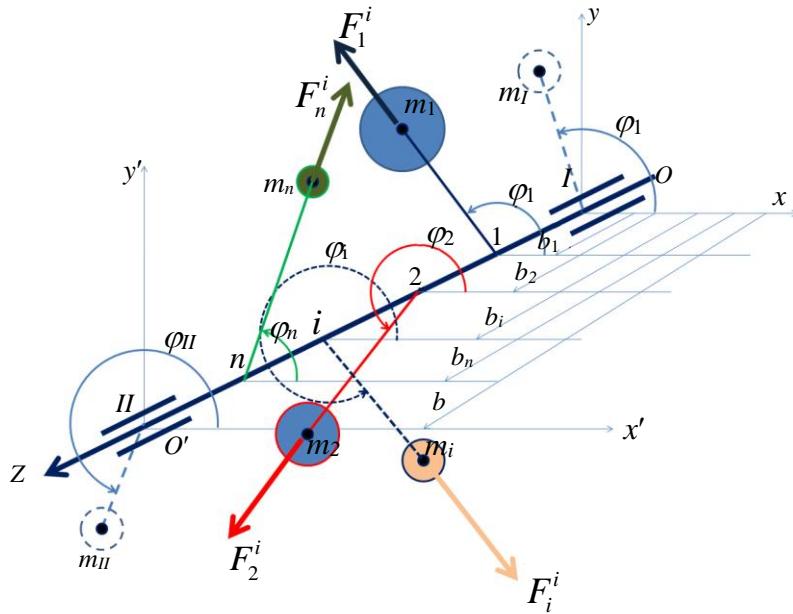


Fig. 9: Balancing of the rotating concentrated masses

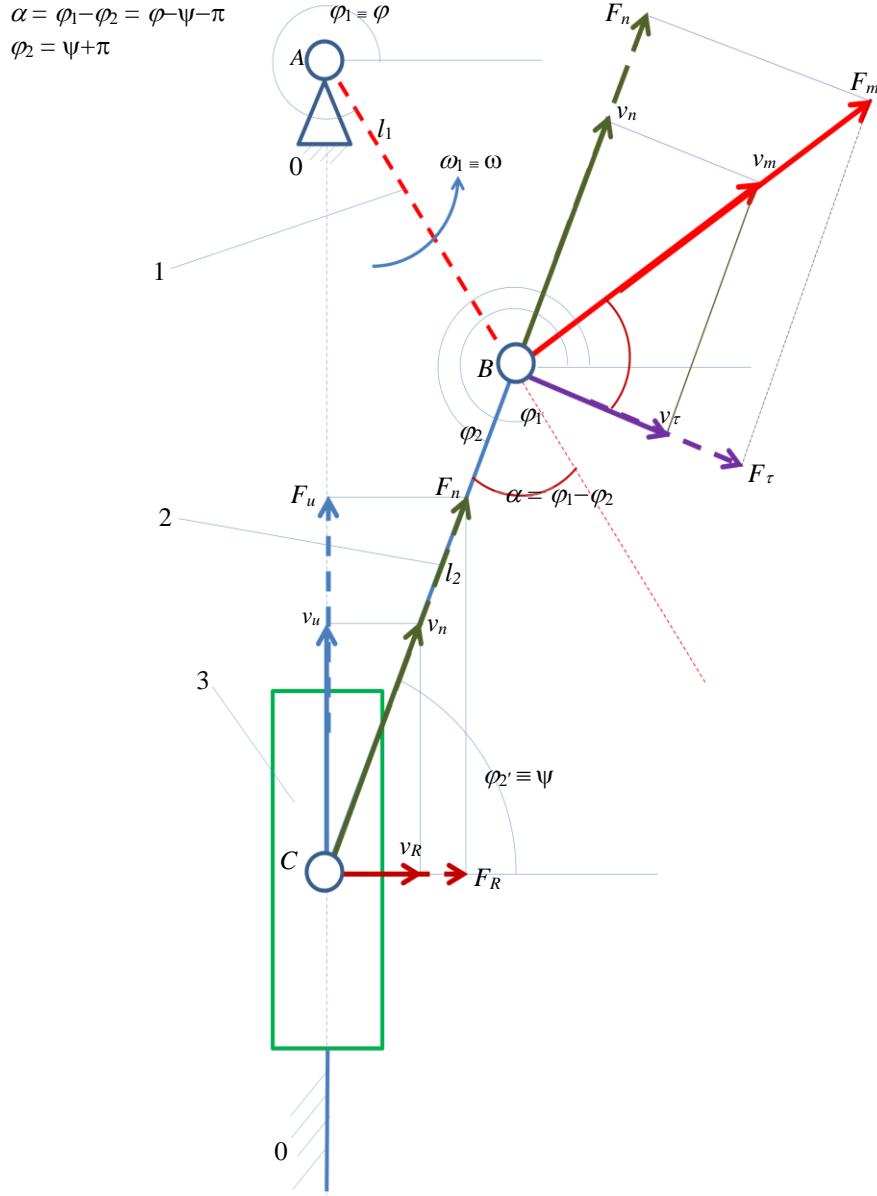


Fig. 10: The distribution of the forces and velocities in engine mechanism, when it is operated of the crank (element 1)

So the new engine will work with moments and low power just like a modern dynamic engine that needs very high powers and moments, plus the proposed engine will be very well balanced statically, ie from the point of view of the inertial forces (Fig. 13). If a total dynamic equilibrium (and balancing momentum of inertial forces) is desired, it will move to the kinematic scheme of Figure 14, where the proposed new engine doubles into the mirror (Petrescu and Petrescu, 2014f; 2014g; 2014h; 2014i):

$$\begin{aligned}
 \sum P = 0 \Rightarrow & F_m \cdot l_1 \cdot \omega_1 + M_2^i \cdot \omega_2 + F_{G_2}^{ix} \cdot \dot{x}_{G_2} + \\
 & + F_{G_2}^{iy} \cdot \dot{y}_{G_2} + F_{G_3}^{iy} \cdot \dot{y}_{G_3} + F_R \cdot \dot{y}_C = 0; \quad F_u = -F_R \Rightarrow \\
 \left\{ \begin{array}{l} F_u = \frac{F_m \cdot l_1 \cdot \omega_1 + M_2^i \cdot \omega_2 + F_{G_2}^{ix} \cdot \dot{x}_{G_2} + F_{G_2}^{iy} \cdot \dot{y}_{G_2} + F_C^{iy} \cdot \dot{y}_C}{\dot{y}_C} \\ F_u = F_m \cdot \sin \psi \cdot \sin(\psi - \phi) \end{array} \right. & \\
 \Rightarrow F_m = \frac{F_C^{iy} \cdot \dot{y}_C + M_2^i \cdot \omega_2 + F_{G_2}^{ix} \cdot \dot{x}_{G_2} + F_{G_2}^{iy} \cdot \dot{y}_{G_2}}{\dot{y}_C \cdot \sin \psi \cdot \sin(\psi - \phi) - l_1 \cdot \omega_1} & \\
 M_m = F_m \cdot l_1 &
 \end{aligned} \tag{6}$$

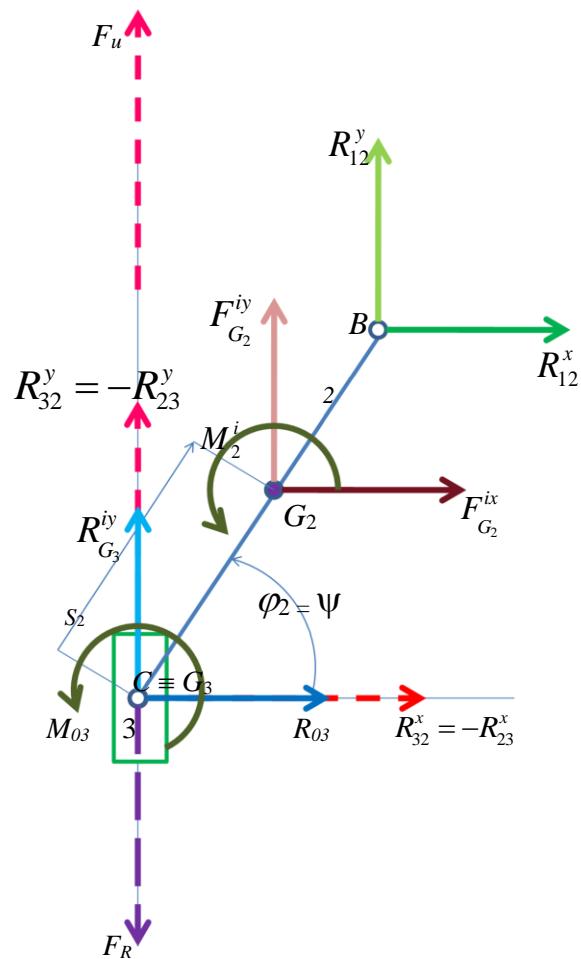


Fig. 11: The forces of mechanism, when it is operated from the crank (element 1)

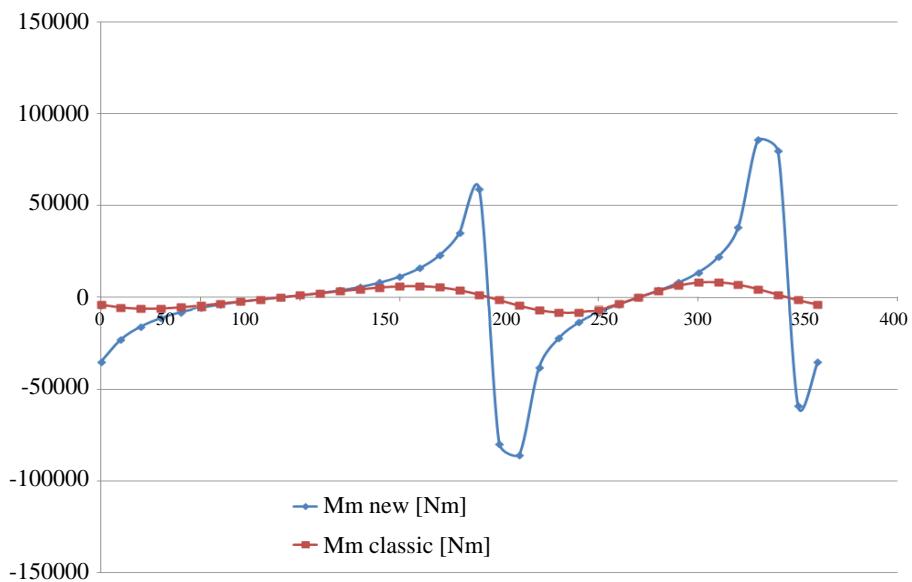


Fig. 12: The classical torque and the new torque

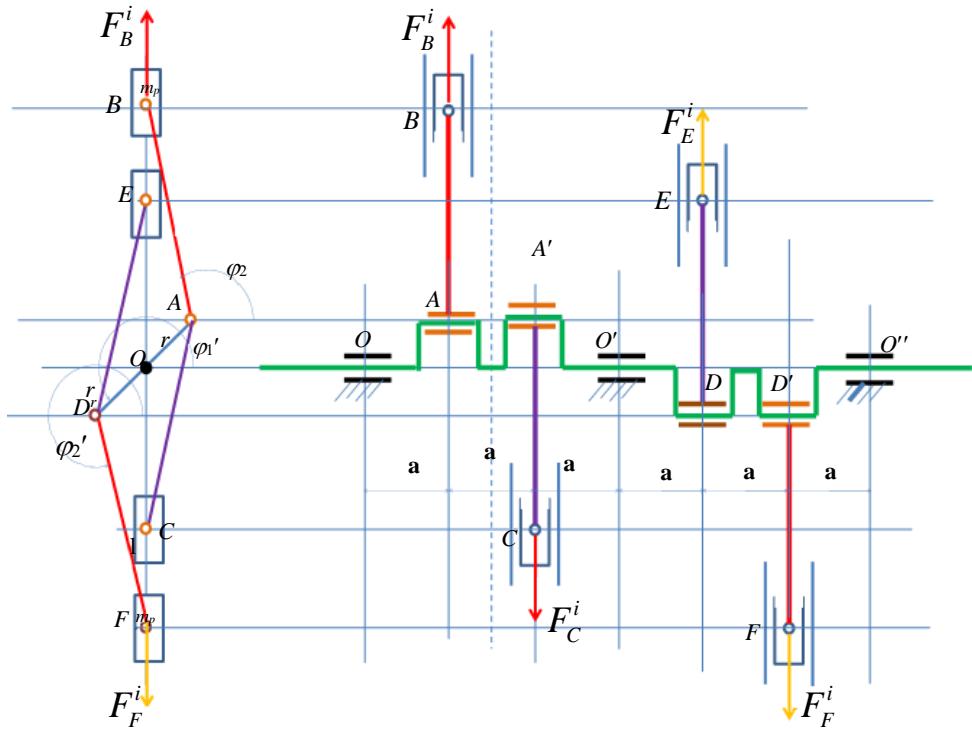


Fig. 13: Balancing of one original internal combustion engine four-cylinder in line

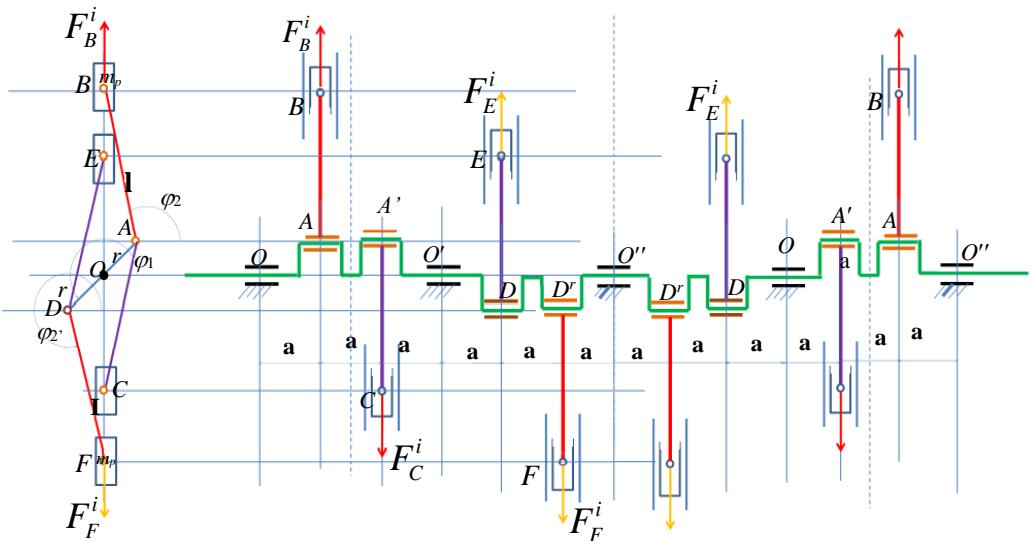


Fig. 14: Balancing of one original internal combustion engine eight-cylinder in line

Conclusion

Today we have a fleet of over one billion vehicles with internal combustion engines such as Otto or diesel, a park that grows every year with another 70-80 million cars, infernal rhythm we could say and all are sold and registered always coming into circulation, because the planet is constantly increasing its population and its

claims to a better life. The problem of fossil fuels and energy has already been solved on a planetary scale, bringing great relief to the entire planet, but the issue of crowding the population on the blue planet has not yet been solved, which is why the permanent improvement of their vehicles and their engines may also it brings many planetary benefits, even if planetary agglomeration will not be solved by this way, but life will still be easier.

A few years ago, a British company managed to get fossil fuels only from the atmosphere and energy, recovering the carbon products existing today in the air. Such a plant has not yet appeared because the technologies are too expensive and we already have fossil reserves at our discretion for several thousand years, given that we have been able to obtain most energy from water, sun, wind or nuclear.

Recently, a prestigious university in Switzerland managed to obtain superior fuels only from water and solar energy through simple, technologically simple processes that will only require a large amount of space allotted to produce continually high-quality kerosene from water and solar energy. So if there are still classical fuels, they can be re-infused just by the water and solar energy. We can now say that the games are already being made, especially as more and more electric motors have appeared on motor vehicles, some of them using hydrogen as a fuel, which in turn is a major energy resource on a massive scale, already massively implemented, and with great prospects for the future.

Under these new conditions, the necessity of continuing the studies on the thermal engines with the aim of their permanent improvement appears.

In order to achieve an optimum and thus have the maximum possible balance of the moments, which would facilitate the optimal operation of the engine at maximum capacity only with reduced moments and powers, so with reduced fuel consumption and low NO_x, it is necessary to pass to a new constructive schema of the internal combustion engine (Fig. 13). So the new engine will work with moments and low power just like a modern dynamic engine that needs very high powers and moments, plus the proposed engine will be very well balanced statically, ie from the point of view of the inertial forces (Fig. 13). If a total dynamic equilibrium (and balancing momentum of inertial forces) is desired, it will move to the kinematic scheme of Figure 14, where the proposed new engine doubles into the mirror.

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All these matters are copyrighted! Copyrights: 394-qodGnhhtej, from 17-02-2010 13:42:18; 463-vpstucGsiy, from 20-03-2010 12:45:30; 631-sqfsgqvutm, from 24-05-2010 16:15:22; 933-CrDztEfqow, from 07-01-2011 13:37:52.

Author's Contributions

All the authors contributed equally to prepare, develop and carry out this manuscript.

Ethics

This article is original and contains unpublished material. Authors declare that there are not ethical issues and no conflict of interest that may arise after the publication of this manuscript.

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Source of Figures:

Petrescu and Petrescu, 2014 f, 2014 g, 2014 h, 2014 i.

Nomenclature

- F_m : is the motor force;
- F_t : is the tangential force, which produces the rotation of the element;
- F_n : is the normal force, which is transmitted along the connecting rod;
- F_R : is the radial force, who press on the cylinder barrel in which guides the piston;
- F_u : The utile force, F_u , moves the piston (when the mechanism is in compressor system) and rotates the crank (when the mechanism is in motor system);
- F_c : is the force of compression and presses on the crankpin (B) and then on the crank and bearing (A);
- $\varphi_1 = \varphi$: is the position angle of the crank;
- $\varphi_2 = \psi$: is the position angle of the rod (element 2), if the rod is considered from the point C;
- $\varphi_2 = \theta$: is the position angle of the rod, if the rod is considered from the point B;
- $\omega_1 = \omega$: the angular rotation speed of the crank (the motor shaft);
- l_1 : is the length of the crank;
- l_2 : is the length of the rod (the connecting rod);
- λ : is the rapport between l_1 and l_2 ;
- η_i^c : is the instantly efficiency of the mechanism in the compressor system;
- η^c : is the mechanical yield of the mechanism in the compressor system;
- η_i^m : is the instantly efficiency of the mechanism in the motor system;
- η^m : is the mechanical yield of the mechanism in the motor system